## ACTIVE APPLICATION ORIENTED LEARNING OF <br> COMPLEX DYNAMICAL SYSTEMS <br> WITH <br> APPLICATION TO MPC

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## The problem



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I'm afraid this still describes state-of-the art....

## Outline

Application oriented experiment design
Output error models
The impact of optimal experiments on the identification problem
Computing the optimal input
Experimental results
Active application oriented learning
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## An application example: MPC of a DC-motor



- Input: Voltage $V$
- Output: Angle $\phi_{L}$
- Model parameters $\theta$ : Resistance $R$, Moment of inertia $J_{L}$, Elasticity $K, \ldots$
- True parameters: $\theta_{o}$


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can approximately be formulated as

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& =\frac{1}{2 \pi} \int_{-\pi}^{\pi} \Phi_{u}^{\mathrm{id}}\left(e^{j \omega}\right)\left|G_{o}\left(e^{j \omega}\right)-G\left(e^{j \omega}, \theta\right)\right|^{2} \mathrm{~d} \omega
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## Output error models

Application oriented experiment design

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Identification cost matched to performance degradation

## Model Reference Control



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- Achieved sensitivity function: $S(G)=\frac{1}{1+C(G) G_{o}}$
- Performance degradation: $V_{\text {app }}(G):=\left\|\frac{S(G)-S_{\xi}}{S_{\xi}}\right\|_{2}^{2}$


## Model Reference Control

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$\Rightarrow N \Phi_{u}^{\text {id }}=\gamma \lambda_{e} n \Phi_{u}^{\text {desired }}$
- Experimental conditions during identification should be a scaled version of the desired operating conditions!


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## Static gain estimation

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Performance degradation: $V_{\text {app }}(\theta)=\left(\sum \theta_{k}-\sum \theta_{k}^{o}\right)^{2}$

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## Application oriented experiment design: Summary

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Aims at achieving

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N V_{\mathrm{id}}(\theta)=\lambda_{e} \gamma n V_{\text {app }}(\theta)
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- Choice of model structure less critical


## Outline

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## Computations: The Information Application Inequality

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The Information Application Inequality
Recall: $V_{\text {id }}$ linear in the input spectrum Information Application Inequality is an LMI in the input spectrum

## Computations

$\min \quad N E\left[u_{t}^{2}\right]$
s.t. $\quad \mathcal{I}_{1}^{N} \succeq \frac{\gamma n}{2} V_{\text {app }}^{\prime \prime}$

## Computations

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white noise



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## Experimental results: Water tank process



## Experimental results: Water tank process



MPC: Black: based on AOID-model. Red: based on white noise excitation

## Computations

Application oriented experiment design

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\begin{array}{ll}
\min N E\left[u^{2}(t)\right] \\
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## Active application oriented learning

white
noise


## Active application oriented learning



## Active application oriented learning



## Active application oriented learning



## Active application oriented learning



- An adaptive feedback system


## Active application oriented learning



- An adaptive feedback system
- But measured signal not fed back directly


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- Exp. design limits input power $\Rightarrow$ Stability when $G_{o}$ stable


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Key questions:

- Convergence?
- Accuracy?


## Active application oriented learning

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## Active application oriented learning

Key questions:

- Convergence?
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## Theorem

- True linear time-invariant system in the model set
- System stable
$\Rightarrow \hat{\theta}(t)$ has the same asymptotic accuracy as the off-line estimate that uses data collected under the optimal experimental conditions (using knowledge of $\theta_{o}$ )


## Active application oriented learning

What happens when true system is not in the model set?

## Example: Non-minimum phase zero estimation

True system: $y_{t}=\frac{(q-3)(q-0.1)(q-0.2)(q+0.3)}{q^{4}(q-0.5)} u_{t}+\frac{q}{q-0.8} e_{t}^{o}$

True system


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Zero estimate


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## Application oriented dual control

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\min _{\text {Input spectrum }} \quad N \mathrm{E}\left[u_{t}^{2}\right], \quad \text { s.t. } \mathcal{I}_{1}^{N}\left(\theta_{o}\right) \succeq \frac{\gamma n}{2} V_{\mathrm{app}}^{\prime \prime}\left(\theta_{o}\right)
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Idéa: Replace cost function with control objective.

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\text { e.g. } y_{t}^{T} Q y_{t}+u_{t} S u_{t}
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$$
\begin{array}{cl}
\min _{\pi} & C_{\beta}(\pi, N) \\
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- Markov Decision Process (MDP) formulation


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We will look at two approaches two solve this problem:

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- Receeding horizon formulation: MPC-X


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$\Rightarrow$ State $x$ \& input $u$ take only finite number of values

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Can be computed based on geometry of discretization and knowledge of distributions of disturbances

Policy: $\pi_{t}(x, u)=\mathbb{P}\left\{u_{t}=u \mid x_{t}=x\right\}$

## Markov Decision Process formulation: Implementation

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\text { s.t. } & N_{\beta}\left(\pi, \theta_{o}\right) \succeq \frac{\gamma n}{2} V_{\mathrm{app}}^{\prime \prime}\left(\theta_{o}\right) \\
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Define $z_{x u}$ as the probability of being in state $x$ and taking action $u$

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Occupancy measure

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Solution?

Define $z_{x u}$ as the probability of being in state $x$ and taking action $u$
Occupancy measure

MDP problem is a semi-definite program in $\left\{z_{x u}\right\}$.

## Markov Decision Process formulation: Simulation study

$$
\left\{\begin{aligned}
x_{t+1} & =-\theta_{1} x_{t}+\theta_{2} u_{t}-\theta_{1} v_{t} \\
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$x$ split in 51 regions.
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c_{t}(x, u)=2 y_{t}^{2}+u_{t}^{2}
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Set of acceptable models: Blue solid ellipse.

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Set of acceptable models: Blue solid ellipse.
Desired confidence ellipsoid: Red dashed ellipse

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Set of acceptable models: Blue solid ellipse.
Desired confidence ellipsoid: Red dashed ellipse
Crosses: 100 Monte Carlo simulations using the MDP controller

## Markov Decision Process formulation: Summary

- Elegant and powerful formulation


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- Leads to a semi-definite program


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- Elegant and powerful formulation
- Leads to a semi-definite program
- but suffers from the curse of dimensionality due to discretization of state-space


## Receeding horizon formulation

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Cost at time $t$ :

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C_{t}=\sum_{k=1}^{F} c_{t}\left(x_{k}, u_{k}\right)=\sum_{k=1}^{F}\left\|y_{k+1}-r_{t+k+1}\right\|_{Q}^{2}+\sum_{k=1}^{F}\left\|u_{k}\right\|_{S}^{2}
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Scaling $\kappa_{t}$ monotonically increasing from 0 to 1 at $t=N-N_{I}$

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Major problems:

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$\Rightarrow$ Cannot use spectrum as design variable


## Receeding horizon formulation: Implementation

Approximations:

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Quadratic in design variables $\bar{u}=\left[u_{1}, \ldots, u_{F}\right]^{T}$

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\text { Quadratic in design variables } \bar{u}=\left[u_{1}, \ldots, u_{F}\right]^{T}
$$

Lifting: Introduce $U=\bar{u} \bar{u}^{T} \Leftrightarrow$

$$
\left[\begin{array}{cc}
U & \bar{u} \\
\bar{u}^{T} & 1
\end{array}\right] \succeq 0, \quad \operatorname{rank}\left[\begin{array}{cc}
U & \bar{u} \\
\bar{u}^{T} & 1
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$$

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- $I_{1}^{N}(\hat{\theta})$ sample approximation of $\mathcal{I}_{1}^{N}\left(\theta_{o}\right)$

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\text { Quadratic in design variables } \bar{u}=\left[u_{1}, \ldots, u_{F}\right]^{T}
$$

Lifting: Introduce $U=\bar{u} \bar{u}^{T} \Leftrightarrow$

$$
\left[\begin{array}{cc}
U & \bar{u} \\
\bar{u}^{T} & 1
\end{array}\right] \succeq 0, \quad \operatorname{rank}\left[\begin{array}{cc}
U & \bar{u} \\
\bar{u}^{T} & 1
\end{array}\right]=1
$$

Convex relaxation: Drop the rank constraint

## Receeding horizon formulation: Implementation

Approximations:

- Initial estimate $\hat{\theta}$ replaces $\theta_{o}$
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Alternative formulation: Minimum time

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Convex relaxation: Drop the rank constraint
Alternative formulation: Minimum time (maximize $\kappa_{t}$ )
MPC-X: Model Predictive Control with eXperimental constraints

## Receeding horizon formulation: Alternative approaches

$$
y_{t}=\sum_{k=1}^{n_{b}} \theta_{k} u_{t-k}+e_{t}=\theta^{T} \phi_{t}+e_{t}
$$

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\end{array}\right]^{T}
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Persistence of excitation condition: $\sum_{k=t-P}^{t+1+F} \phi_{k} \phi_{k}^{T} \succeq \rho I$

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- MPCI (Genceli and Nikolaou (1996)): $P=0$
- Multiobjective MPC with identification (Aggelogiannaki and Sarimveis (2006)): $P=0$
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- PE-MPC (Marafioti (2010)): $F=0$


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Do not take application into account explicitly

## Receeding horizon formulation: Simulation study



## Receeding horizon formulation: Simulation study

$$
\left\{x_{t+1}=\left[\begin{array}{cc}
\theta_{3} & \theta_{4} \\
1 & 0
\end{array}\right] x_{t}+\left[\begin{array}{c}
4.5 \\
0
\end{array}\right] u_{t}\right.
$$

## Receeding horizon formulation: Simulation study

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0
\end{array}\right] u_{t}, \\
y_{t} & =\left[\begin{array}{ll}
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\end{array}\right] x_{t}+e_{t}
\end{aligned}\right.
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y_{t} & =\left[\begin{array}{ll}
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\end{array}\right] x_{t}+e_{t} \quad \text { lower tank level }
\end{aligned}\right.
$$

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\theta_{o}=\left[\begin{array}{lll}
0.12 & 0.059 & 0.74 \\
-0.14
\end{array}\right]^{T} \quad \text { Noise var.: } 0.01 . \\
N=200, \quad F=5
\end{array}\right.
\end{aligned}
$$

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\end{aligned}
$$

Performance degradation cost: $V_{\text {app }}(\theta)=\sum_{t=1}^{T}\left\|y_{t}\left(\theta_{o}\right)-y_{t}(\theta)\right\|_{2}^{2}$

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& N
\end{aligned}=200, \quad F=5-5=2
$$

Performance degradation cost: $V_{\text {app }}(\theta)=\sum_{t=1}^{T}\left\|y_{t}\left(\theta_{o}\right)-y_{t}(\theta)\right\|_{2}^{2}$
PE-MPC: $\rho=0.5, P=5, F=0$

## Receeding horizon formulation: Simulation study

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PE-MPC: $\rho=0.5, P=5, F=0$
MPC-X: Minimum time formulation

Receeding horizon formulation: Simulation study

$$
\begin{aligned}
& \text { Time (sample) }
\end{aligned}
$$

## Receeding horizon formulation: Simulation study





## Receeding horizon formulation: Simulation study



- Regular MPC (-),
- PE-MPC with $\rho=0.5(-)$
- Minimum time MPC-X (-)


## Receeding horizon formulation: Simulation study

| Algorithm | $\operatorname{Var} u$ | $\operatorname{Var} y$ | $N$ |
| :--- | :---: | :---: | :---: |
| MPC-X, minimum time | 0.203 | 0.146 | 82 |
| PE-MPC, $\rho=0.5$ | 0.175 | 0.120 | 211 |

## MPC-X experimental study: Let's travel



## Secunda, South Africa



## SASOL Synthetic Fuels Refinery



## Synfuels Catalytic Cracker (SCC)



## Depropanizer



## Depropanizer

Separates three-carbon hydrocarbons $\left(C_{3}\right)$ from four carbon hydrocarbons ( $C_{4}$ )

Objective: Set point for $\mathrm{CV} 1=C_{4}$ concentration in side draw MV2: Side draw to feed ratio

MV3: Column differential pressure

## Depropanizer

Separates three-carbon hydrocarbons $\left(C_{3}\right)$ from four carbon hydrocarbons ( $C_{4}$ )

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Performance drop obtained by changing poles of model

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Separates three-carbon hydrocarbons $\left(C_{3}\right)$ from four carbon hydrocarbons ( $C_{4}$ )

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MV3: Column differential pressure
Performance drop obtained by changing poles of model
Excitation level manually controlled

## Depropanizer: MPC-X experiment






## Depropanizer: Model fit

Open loop data


Closed loop data


- The plant output (-)
- Model identified in open-loop (-)
- Model identified in closed-loop MPC-X experiment (-)


## Depropanizer: Closed loop performance

|  | Variance |  |
| ---: | ---: | ---: |
| Model | CV 1 | MV 5 |
| Before MPC-X | $95 \times 10^{3}$ | $34 \times 10^{7}$ |
| After MPC-X model update | $36 \times 10^{3}$ | $37 \times 10^{7}$ |

$\mathrm{MV} 5=C_{4}$ content in the feed

## MPC-X: Summary

- Sample version of Information Application Inequality added as a matrix inequality constraint in MPC


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- Convex relaxation


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- Sample version of Information Application Inequality added as a matrix inequality constraint in MPC
- Convex relaxation
- Current limitation: Output error models (disturbances not modeled)


## Outline

Application oriented experiment design
Output error models
The impact of optimal experiments on the identification problem
Computing the optimal input
Experimental results
Active application oriented learning
Application oriented dual control
Summary

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## What have we learnt?

- A framework for experiment design where the application is taken into account
- The optimal experiment matches the identification criterion to the performance degradation using parsimonious excitation
(The let sleeping dogs lie paradigm)
- Simplifies the identification problem
- Active application oriented learning practical implementation
- Adding the Information Application Inequality to an optimal control problem leads to dual control


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## Active Application Oriented Learning

THANK YOU!!!

